

Expert Group Meeting

「高エネルギー粒子，加熱および定常運転」理論関係報告

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International Workshop on Physics of Internal Transport Barrier,
Edge Pedestal and Steady State Operation in Tokamaks
IPP Garching, Germany, 2001/04/23-27

- 高エネルギー粒子 : Zonca, Jaun, Fukuyama
- 加熱 : Fukuyama, Prater, Vdovin
- 定常運転 :
- コメント

Zonal Flow Excitation by Nonlinear EPM Dynamics

F. Zonca (ENEA, Frascati)

- 3D Hybrid MHD-Gyrokinetic code による
EPM の非線形シミュレーション
 - Briguglio et al. PoP 2 (1995) 3711; PoP 5 (1998) 3287
 - EPM の非線形発展と粒子輸送
 - EPM の励起がしきい値を越えると
 - 高速粒子の分布が径方向に再分配され
 - モードが飽和する .
 - $n = 8$ EPM: $\beta_{E0} = 0.75 \%$, $L_{pE}/R_0 \simeq 0.075$, $\rho_{LE}/a = 0.01$
 - EPM による渦構造が径方向に分裂 ($k_\theta = k_{\parallel} = 0$)
 - 高速イオンの拡散的輸送
- 变調不安定性と EPM 渦の径方向分裂 (analytic)
 - pump EPM \pm zonal flow = sidebands

Alfvén Eigenmode Experiments on JET

A. Jaun (Alfvén Lab)

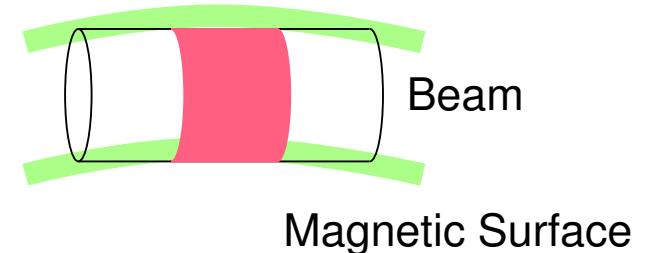
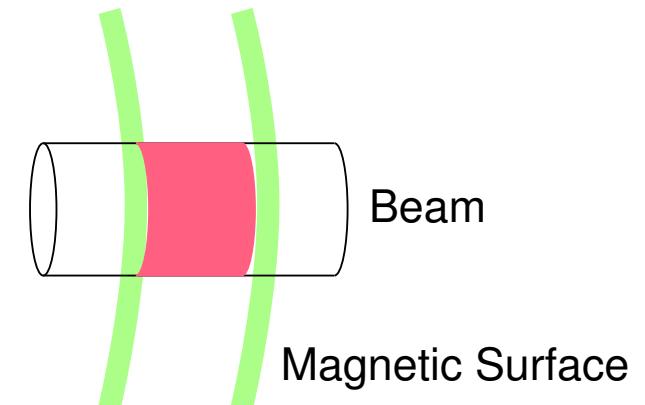
- これまでの理解 : PENN code
 - アルヴェン固有モードの安定性はモード変換が支配
 - ダイバータ配位における X 点近傍の安定化効果
- パラメータ依存性
 - 反転磁気シア : 安定化 / 不安定化ははっきりしない .
 - β 依存性 : β の増加とともに中心部の減衰増大 : KTAE?
 - B 依存性 : 減衰率は B に依存せず . Radiative damping ではない .
 - q_0 依存性 : $q_0 > 5$ の場合 , I_{rp} に依存しない低減衰率モード出現
Drift-kinetic Alfvén eigemodes?
- ITER に対する検討事項
 - 実験データと理論モデルとの定量的比較
 - 高 q_0 プラズマにおいて出現する低減衰モードの影響

加熱・電流駆動・定常運転

- EC:
 - Fukuyama: Evaluation of Radial Deposition width in ECCD
 - Prater: Progress on ECH and ECCD in DIII-D
 - 電子の β 値とともに電流駆動効率増加（理論と一致）
 - 小半径の大きな領域や異なる入射角での実験が必要
- IC
 - Vdovin: ICRF シナリオ in ITER

Motivation

- Current profile control by EC waves
 - Localized profile of driven current
 - Position control by injection angle
- Control of MHD instability
 - Suppression of island growth due to tearing instability
 - Localized current profile is required
- Evaluation of the current profile width
 - Doppler broadening, decay length
 - Finite beam size, focusing
 - Defraction
- Limitation of ray tracing
 - Defraction effect cannot be included



Beam Tracing Method

- Beam size perpendicular to the beam direction: first order in δ
- Beam shape : Weber function Hermite polynomial: H_n)

$$E(\mathbf{r}) = \operatorname{Re} \left[\sum_{mn} C_{mn} (\delta^2 \mathbf{r}) e(\delta^2 \mathbf{r}) H_m(\delta \xi_1) H_n(\delta \xi_2) e^{i s(\mathbf{r}) - \phi(\mathbf{r})} \right]$$

- Amplitude : C_{mn} , Polarization : e , Phase : $s(\mathbf{r}) + i\phi(\mathbf{r})$

$$s(\mathbf{r}) = s_0(\tau) + k_\alpha^0(\tau)[r^\alpha - r_0^\alpha(\tau)] + \frac{1}{2}s_{\alpha\beta}[r^\alpha - r_0^\alpha(\tau)][r^\beta - r_0^\beta(\tau)]$$

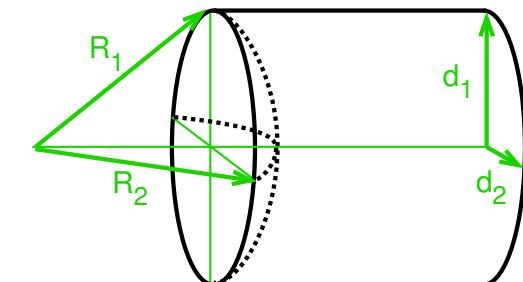
$$\phi(\tau) = \frac{1}{2}\phi_{\alpha\beta}[r^\alpha - r_0^\alpha(\tau)][r^\beta - r_0^\beta(\tau)]$$

- Position of beam axis : r_0 , Wave number on beam axis: k^0

- Curvature radius of equi-phase surface: $R_\alpha = \frac{1}{\lambda s_{\alpha\alpha}}$

- Beam radius : $d_\alpha = \sqrt{\frac{2}{\phi_{\alpha\alpha}}}$

- Gaussian beam : case with $m = 0, n = 0$



Beam Propagation Equation

- Solvable condition for Maxwell's equation with beam field

$$\frac{dr_0^\alpha}{d\tau} = \frac{\partial K}{\partial k_\alpha}$$

$$\frac{dk_\alpha^0}{d\tau} = -\frac{\partial K}{\partial r^\alpha}$$

$$\frac{ds_{\alpha\beta}}{d\tau} = -\frac{\partial^2 K}{\partial r^\alpha \partial r^\beta} - \frac{\partial^2 K}{\partial r^\beta \partial k_\gamma} s_{\alpha\gamma} - \frac{\partial^2 K}{\partial r^\alpha \partial k_\gamma} s_{\beta\gamma} - \frac{\partial^2 K}{\partial k^\gamma \partial k^\delta} s_{\alpha\gamma} s_{\beta\delta} + \frac{\partial^2 K}{\partial k^\gamma \partial k^\delta} \phi_{\alpha\gamma} \phi_{\beta\delta}$$

$$\frac{d\phi_{\alpha\beta}}{d\tau} = -\left(\frac{\partial^2 K}{\partial r^\alpha \partial k^\gamma} + \frac{\partial^2 K}{\partial k^\gamma \partial k_\delta} s_{\alpha\delta}\right) \phi_{\beta\gamma} - \left(\frac{\partial^2 K}{\partial r^\beta \partial k^\gamma} + \frac{\partial^2 K}{\partial k^\gamma \partial k_\delta} s_{\beta\delta}\right) \phi_{\alpha\gamma}$$

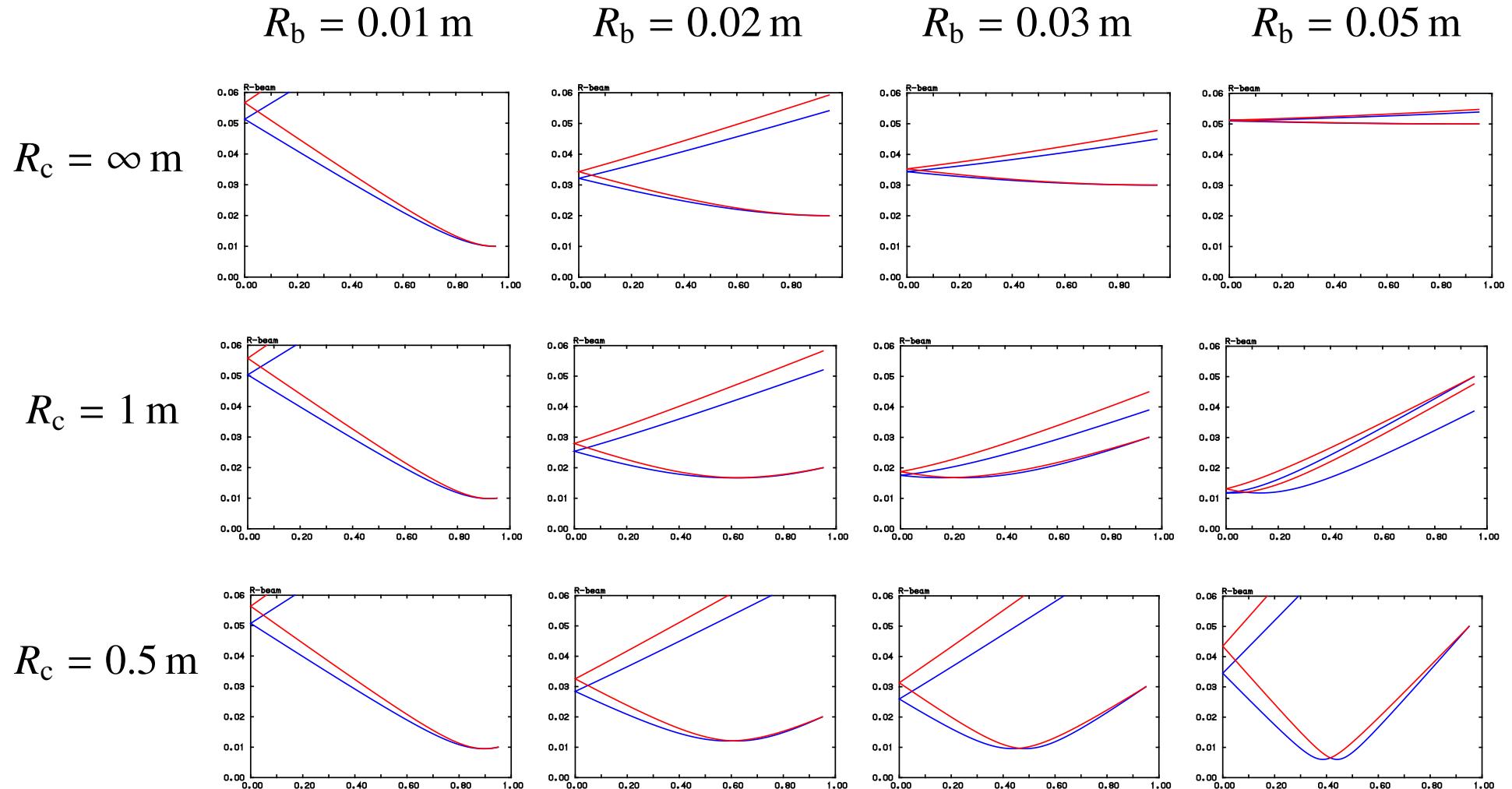
- By integrating this set of 18 ordinary differential equations, we obtain trace of the beam axis, wave number on the beam axis, curvature of equi-phase surface, and beam size.
- Equation for the wave amplitude C_{mn}

$$\nabla \cdot (v_{g0} |C_{mn}|^2) = -2 (\gamma |C_{mn}|^2)$$

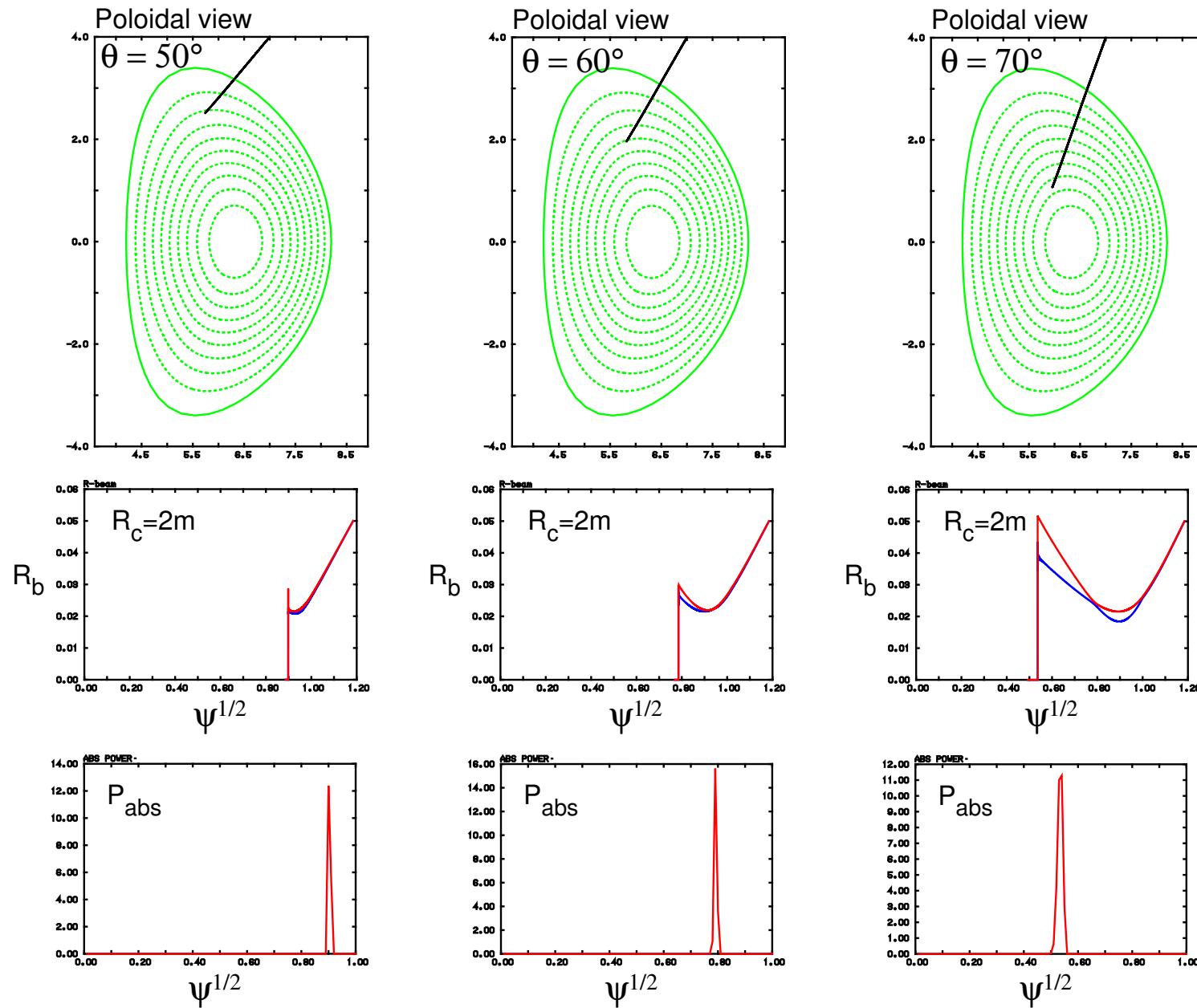
Group velocity: v_{g0} , Damping rate: $\gamma \equiv (\mathbf{e}^* \cdot \vec{\epsilon}_A \cdot \mathbf{e}) / (\partial K / \partial \omega)$

Beam Tracing in a Uniform Plasma

- 160 GHz, Ordinary Mode, Perpendicular Injection



Beam Tracing in ITER-FEAT Plasma



Summary

- Based on the formulation of beam tracing, the wave propagation code TASK/WR was extended to calculate the spatial evolution of the EC beam size.
- We have confirmed the diffraction effect and the initial wave front curvature dependence of the beam size.
- In order to focus after 1 m propagation, initial beam radius of 3cm is required for 160 GHz.
- In the case of ITER-FEAT, initial beam radius of 5cm is required to focus in the NTM island region.
- To dos:
 - Magnetic surface average
 - Coupling with Fokker-Planck Analysis

コメント

- IAEA Fusion Energy Conf. 2002 に予定されている論文題目
 - Collective modes and Fast Particle effects on ITER
 - Progress on Steady State scenarios for ITER
- 今後の課題（理論・シミュレーション）
 - 高速粒子
 - アルヴェン固有モードの安定性
(負磁気シア配位, EPM, ドリフト波との結合)
 - アルヴェン固有モードによる非線形効果(飽和, バースト, 再分配)
 - 定常運転
 - ECCD による NTM の安定化
 - 輸送障壁：エッジ温度, 内部輸送障壁
 - 粒子輸送：密度限界, 不純物輸送, 燃料補給