

Integrated Full Wave Analysis of RF Heating and Current Drive in Toroidal Plasmas

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Outline

- Present Status of TASK Code
- Full wave analysis of ECH in small ST
- Self-consistent analysis of wave heating and current drive
- Integral formulation of full wave analysis
- Summary

Motivation

- **Full wave analysis is required in various situations in tokamaks and helical systems**
 - **Ion cyclotron wave** : wavelength $\sim$ inhomogeneous scale length
 - **Lower hybrid wave** : effect of multiple reflections
 - **Electron cyclotron wave** : tunneling through a cutoff layer
- **Further extension is required for integrated analysis**
 - **Consistent analysis including the modification of $f_0(v)$**
 - **Application to high-frequency waves**
 - **Precise analysis including the FLR effects**
- **Integrated analysis using the TASK code**

TASK Code

- **Transport Analysing System for Tokamak**
- **Features**
 - **A Core of Integrated Modeling Code in BPSI**
 - Modular structure, Unified Standard data interface
 - **Various Heating and Current Drive Scheme**
 - EC, LH, IC, AW, (NB)
 - **High Portability**
 - Most of Library Routines Included
 - **Development using CVS** (Concurrent Version System)
 - Open Source (V0.93 <http://bpsi.nucleng.kyoto-u.ac.jp/task/>)
 - **Parallel Processing using MPI Library**
 - **Extension to Toroidal Helical Plasmas**

Modules of TASK

EQ	2D Equilibrium	Fixed/Free boundary, Toroidal rotation
TR	1D Transport	Diffusive transport, Transport models
WR	3D Geometr. Optics	EC, LH: Ray tracing, Beam tracing
WM	3D Full Wave	IC, AW: Antenna excitation, Eigen mode
FP	3D Fokker-Planck	Relativistic, Bounce-averaged
DP	Wave Dispersion	Local dielectric tensor, Arbitrary $f(v)$
PL	Data Interface	Data conversion, Profile database
LIB	Libraries	

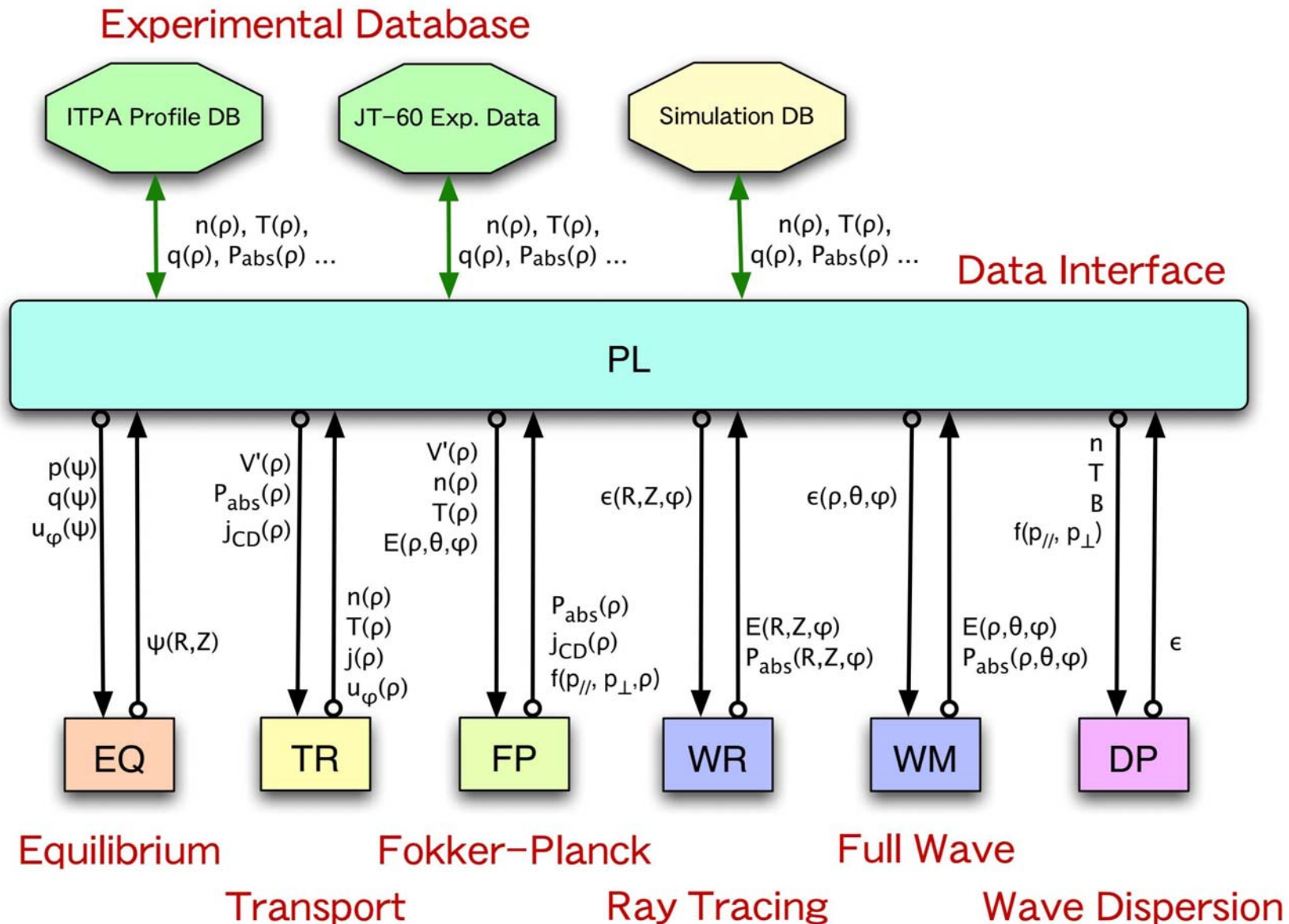
under development

TX	Transport analysis including plasma rotation and E_r
WA	Global linear stability analysis

in collaboration

TOPICS-EQU	Free-boundary equilibrium: Azumi (JAEA)
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Modular Structure of TASK



Wave Dispersion Analysis : TASK/DP

- **Various Models of Dielectric Tensor** $\overleftrightarrow{\epsilon}(\omega, \mathbf{k}; r)$:
 - **Resistive MHD** model
 - **Collisional cold** plasma model
 - **Collisional warm** plasma model
 - **Kinetic plasma** model (**Maxwellian**, non-relativistic)
 - **Kinetic plasma** model (**Arbitrary** $f(v)$, relativistic)
 - **Gyro-kinetic plasma** model (Maxwellian)
- **Numerical Integration in momentum space**: **Arbitrary** $f(v)$
 - Relativistic Maxwellian
 - Output of TASK/FP: Fokker-Planck code

Full wave analysis: TASK/WM

- **magnetic surface coordinate**: (ψ, θ, φ)

- Boundary-value problem of **Maxwell's equation**

$$\nabla \times \nabla \times \mathbf{E} = \frac{\omega^2}{c^2} \overleftrightarrow{\epsilon} \cdot \mathbf{E} + i \omega \mu_0 \mathbf{j}_{\text{ext}}$$

- Kinetic **dielectric tensor**: $\overleftrightarrow{\epsilon}$

- **Wave-particle resonance**: $Z[(\omega - n\omega_c)/k_{\parallel}v_{\text{th}}]$

- **Fast ion: Drift-kinetic**

$$\left[\frac{\partial}{\partial t} + v_{\parallel} \nabla_{\parallel} + (\mathbf{v}_d + \mathbf{v}_E) \cdot \nabla + \frac{e_{\alpha}}{m_{\alpha}} (v_{\parallel} E_{\parallel} + \mathbf{v}_d \cdot \mathbf{E}) \frac{\partial}{\partial \varepsilon} \right] f_{\alpha} = 0$$

- Poloidal and toroidal **mode expansion**

- **Accurate estimation of $k_{\parallel}$**

- Eigenmode analysis: **Complex eigen frequency** which maximize wave amplitude for fixed excitation proportional to electron density

Full Wave Analysis of ECH in a Small-Size ST

- **Small-size spherical tokamak: LATE** (Kyoto University)
 - **T. Maekawa et al., IAEA-CN-116/EX/P4-27 (Vilamoura, Portugal, 2004)**
 - $R = 0.22$ m, $a = 0.16$ m, $B_0 = 0.0552$ T, $I_p = 6.25$ kA, $\kappa = 1.5$
 - $f = 2.8$ GHz, Toroidal mode number $n = 12$, Extraordinary mode

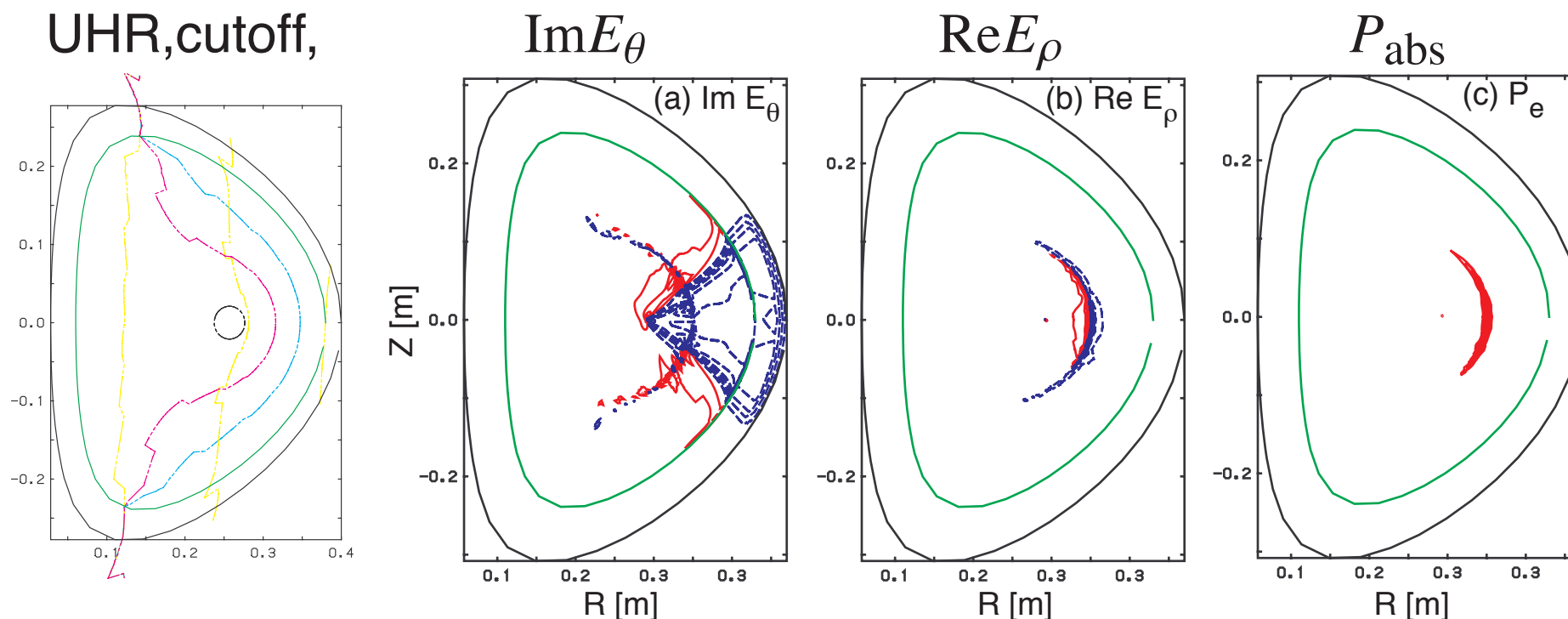
Penetration
through cutoff layer



Propagation
along the UHR layer



Collisional damping
near the UHR layer



Density Dependence of ECW Propagation

LATE: 5 GHz, 0.072 T, $N_{\parallel} = 0.5$

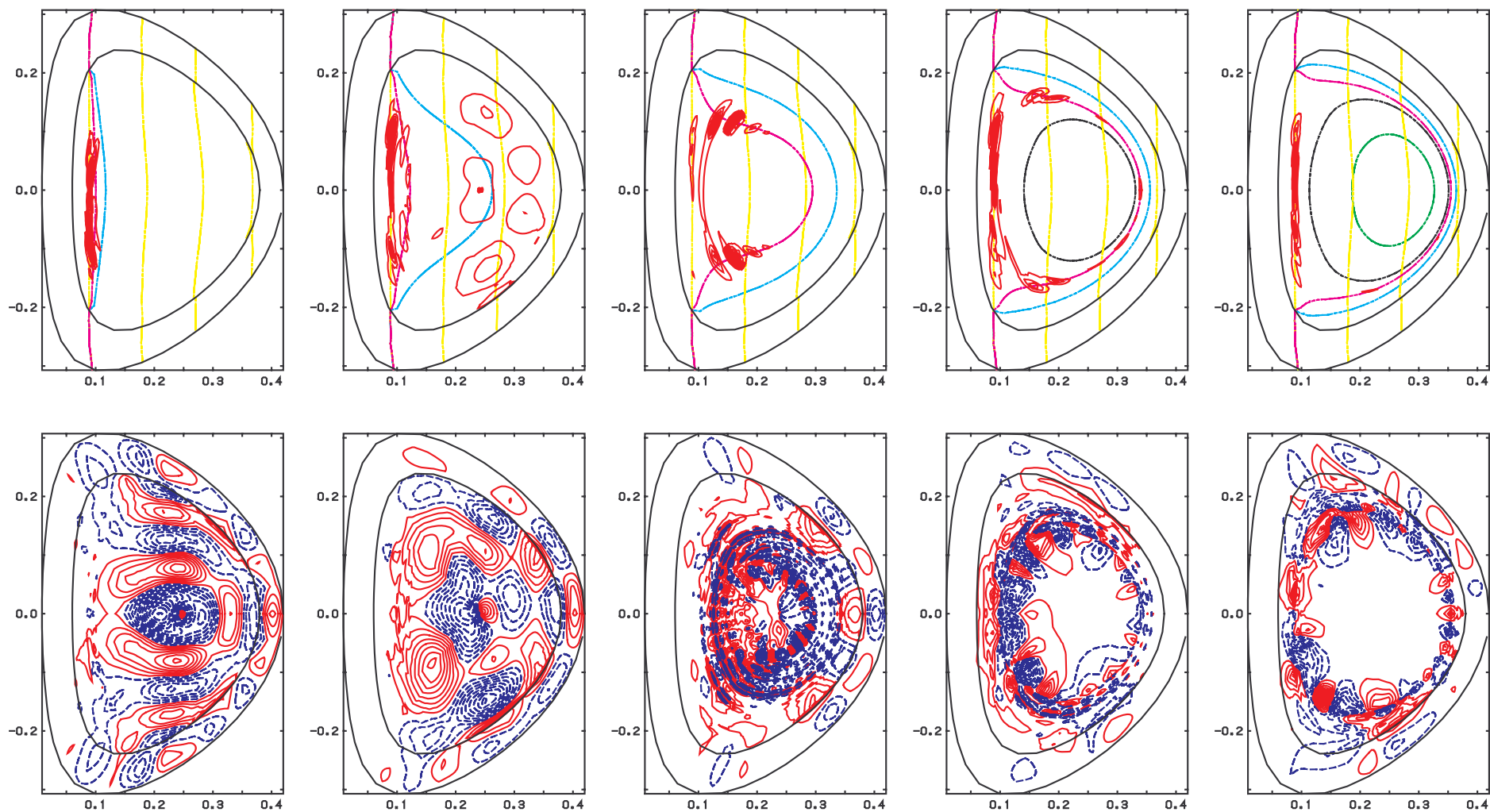
10^{17} m^{-3}

$2 \times 10^{17} \text{ m}^{-3}$

$3 \times 10^{17} \text{ m}^{-3}$

$4 \times 10^{17} \text{ m}^{-3}$

$5 \times 10^{17} \text{ m}^{-3}$



Fokker-Planck Analysis : TASK/FP

- **Fokker-Planck equation**

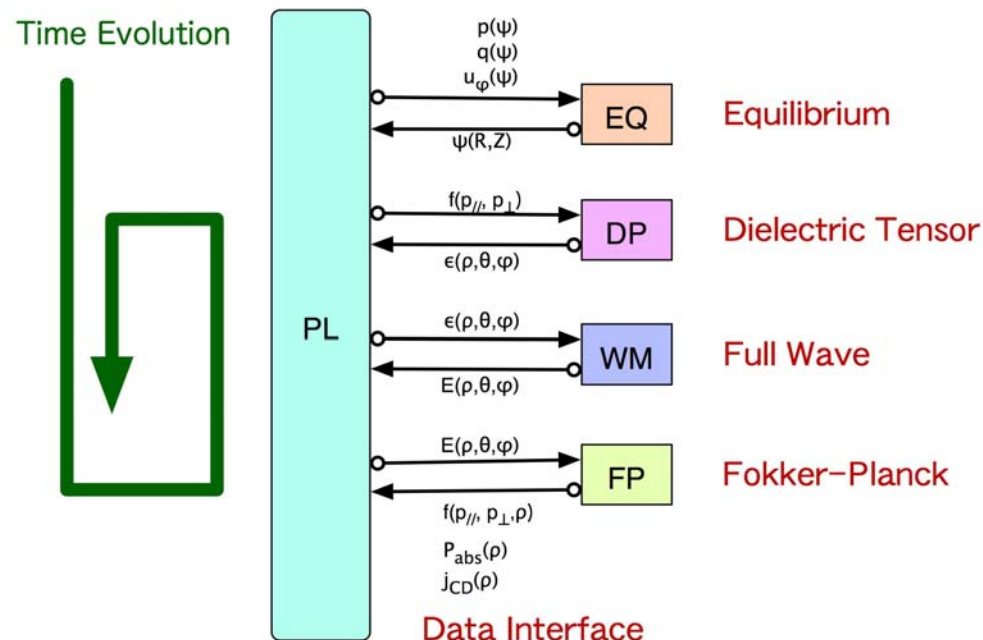
for **velocity distribution function** $f(p_{\parallel}, p_{\perp}, \psi, t)$

$$\frac{\partial f}{\partial t} = E(f) + C(f) + Q(f) + L(f)$$

- $E(f)$: Acceleration term due to DC electric field
 - $C(f)$: Coulomb collision term
 - $Q(f)$: Quasi-linear term due to wave-particle resonance
 - $L(f)$: Spatial diffusion term
- **Bounce-averaged**: Trapped particle effect, zero banana width
 - **Relativistic**: momentum p , weakly relativistic collision term
 - **Nonlinear collision**: momentum or energy conservation
 - **Three-dimensional**: spatial diffusion (neoclassical, turbulent)

Self-Consistent Wave Analysis with Modified $f(v)$

- **Modification of velocity distribution from Maxwellian**
 - Absorption of ICRF waves in the presence of energetic ions
 - Current drive efficiency of LHCD
 - NTM controllability of ECCD (absorption width)
- **Self-consistent wave analysis including modification of $f(v)$**



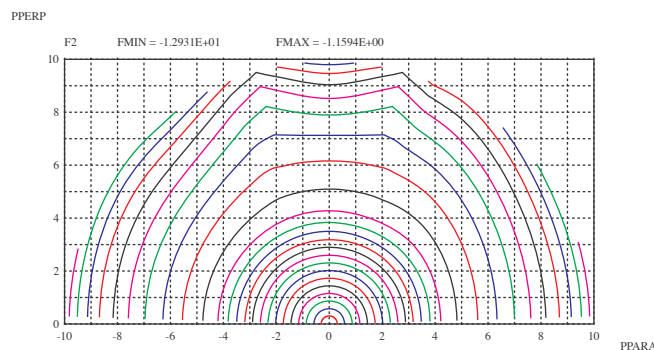
Development of Self-Consistent Wave Analysis

- **Code Development in TASK**

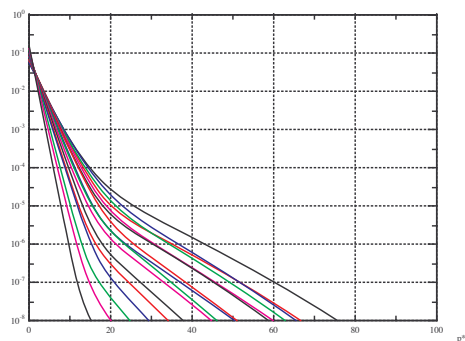
- Ray tracing analysis with arbitrary $f(v)$: **Already done**
- Full wave analysis with arbitrary $f(v)$: **Completed**
- Fokker-Plank analysis of ray tracing results: **Already done**
- Fokker-Plank analysis of full wave results: **Almost completed**
- Self-consistent iterative analysis: **Preliminary**

- **Tail formation by ICRF minority heating**

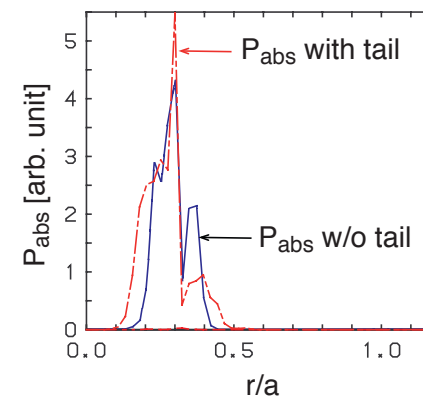
Momentum Distribution



Tail Formation



Power deposition



FLR Effects in Full Waves Analyses

- Several approaches to describe the FLR effects.
- **Differential operators:** $k_{\perp}\rho \rightarrow i\rho\partial/\partial r_{\perp}$
 - This approach cannot be applied to the case $k_{\perp}\rho \gtrsim 1$.
 - Extension to the third and higher harmonics is difficult.
- **Spectral method:** Fourier transform in inhomogeneous direction
 - This approach can be applied to the case $k_{\perp}\rho > 1$.
 - All the wave field spectra are coupled with each other.
 - Solving a dense matrix equation requires large computer resources.
- **Integral operators:** $\int \epsilon(x - x') \cdot E(x') dx'$
 - This approach can be applied to the case $k_{\perp}\rho > 1$
 - Correlations are localized within several Larmor radii
 - Necessary to solve a large band matrix

Full Wave Analysis

Using an Integral Form of Dielectric Tensor

- **Maxwell's equation:**

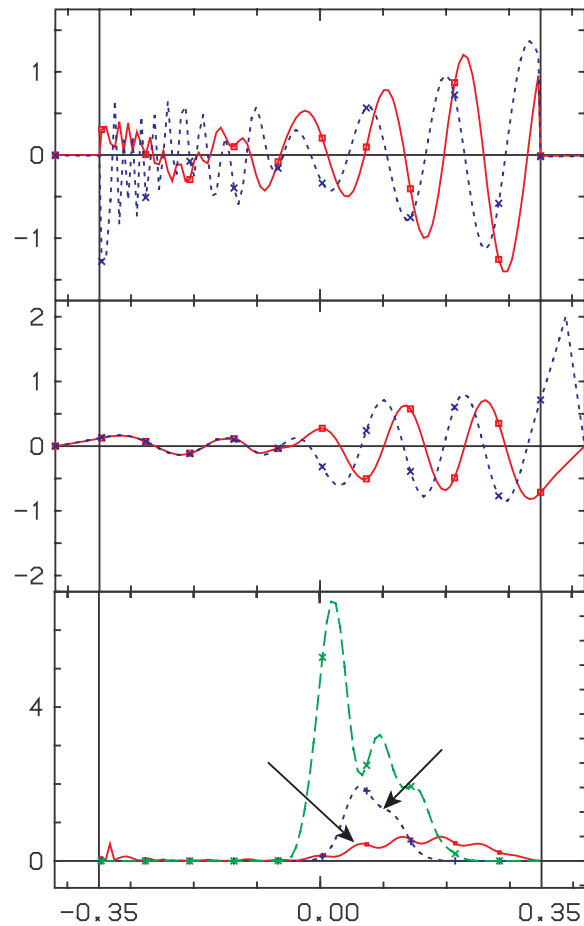
$$\nabla \times \nabla \times \mathbf{E}(\mathbf{r}) + \frac{\omega^2}{c^2} \int \overleftrightarrow{\epsilon}(\mathbf{r}, \mathbf{r}') \cdot \mathbf{E}(\mathbf{r}') d\mathbf{r}' = \mu_0 \mathbf{J}_{ext}(\mathbf{r})$$

- **Integral form of dielectric tensor:** $\overleftrightarrow{\epsilon}(\mathbf{r}, \mathbf{r}')$
 - Integration along the unperturbed cyclotron orbit
- **1D analysis in tokamaks** (in the direction of major radius)
 - To confirm the applicability of an integral form of dielectric tensor
 - **Another formulation in the lowest order of ρ/L**
 - Sauter O, Vaclavik J, Nucl. Fusion **32** (1992) 1455.
- **2D analysis in tokamaks**
 - In more realistic configurations

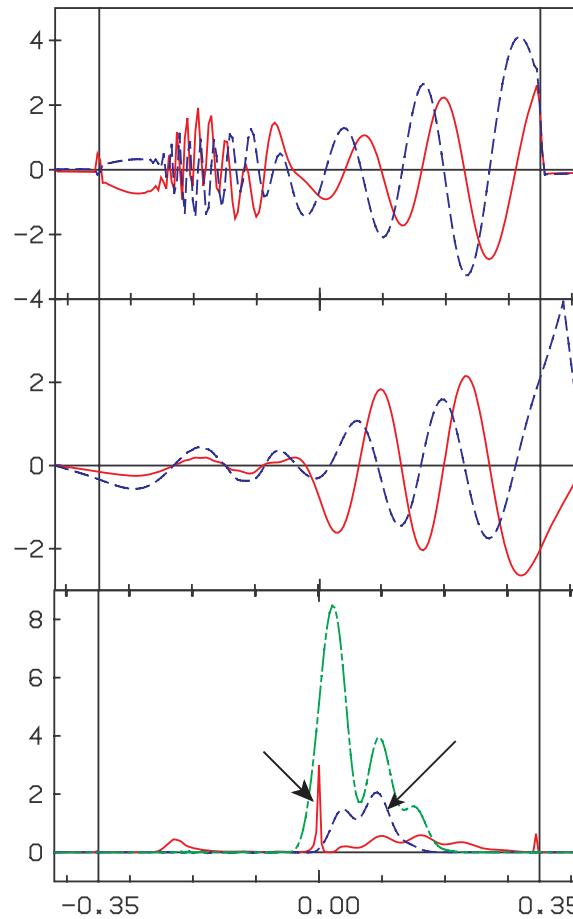
One-Dimensional Analysis (1)

ICRF minoring heating without energetic particles ($n_H/n_D = 0.1$)

Differential form



Integral form



$$R_0 = 1.31\text{m}$$

$$a = 0.35\text{m}$$

$$B_0 = 1.4\text{T}$$

$$T_{e0} = 1.5\text{keV}$$

$$T_{D0} = 1.5\text{keV}$$

$$T_{H0} = 1.5\text{keV}$$

$$n_{s0} = 10^{20}\text{m}^{-3}$$

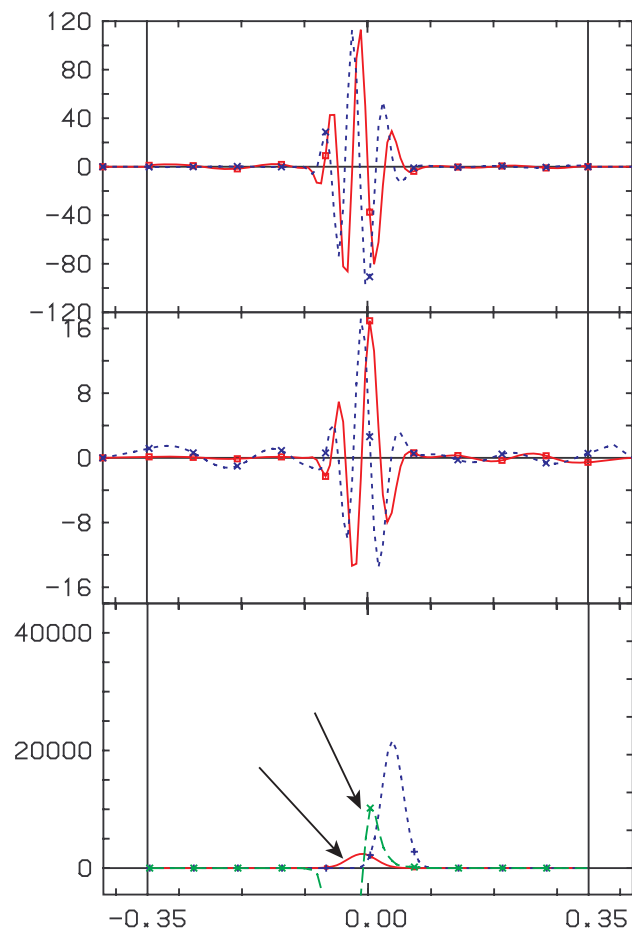
$$\omega/2\pi = 20\text{MHz}$$

Differential approach is applicable

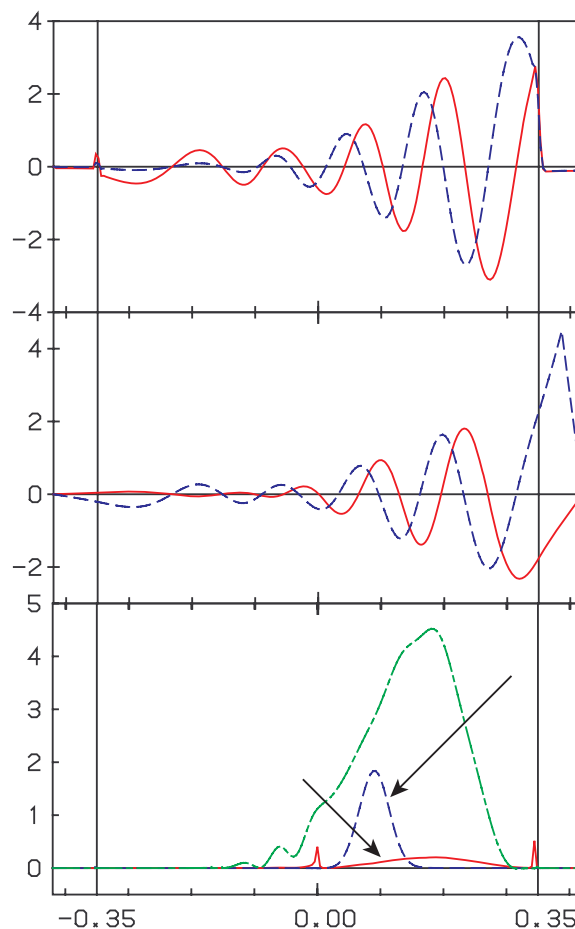
One-Dimensional Analysis (2)

ICRF minoring heating with energetic particles ($n_{\text{H}}/n_{\text{D}} = 0.1$)

Differential form



Integral form



$$R_0 = 1.31\text{m}$$

$$a = 0.35\text{m}$$

$$B_0 = 1.4\text{T}$$

$$T_{e0} = 1\text{keV}$$

$$T_{D0} = 1\text{keV}$$

$$T_{H0} = 100\text{keV}$$

$$n_{s0} = 10^{20}\text{m}^{-3}$$

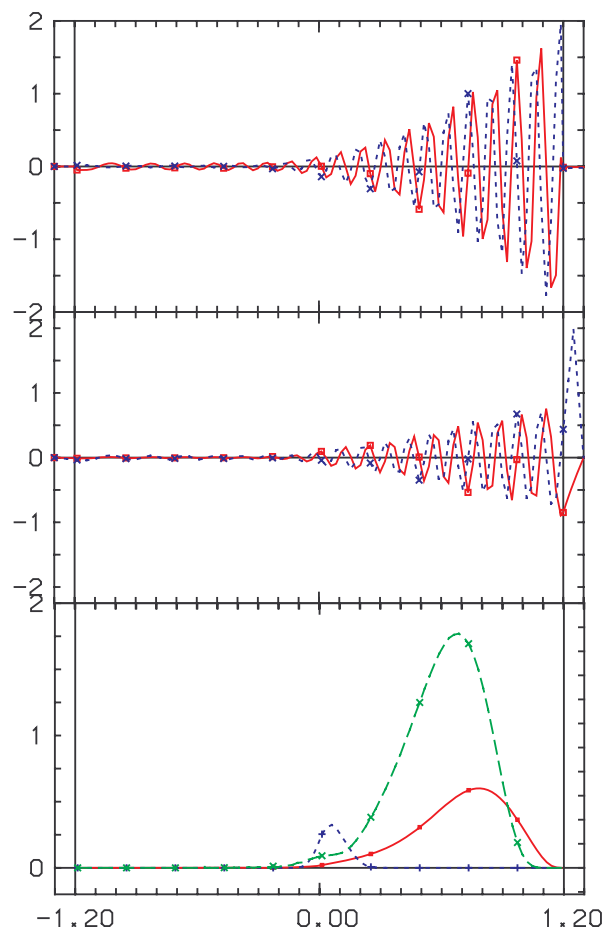
$$\omega/2\pi = 20\text{MHz}$$

Differential approach cannot be applied since $k_{\perp}\rho_i > 1$.

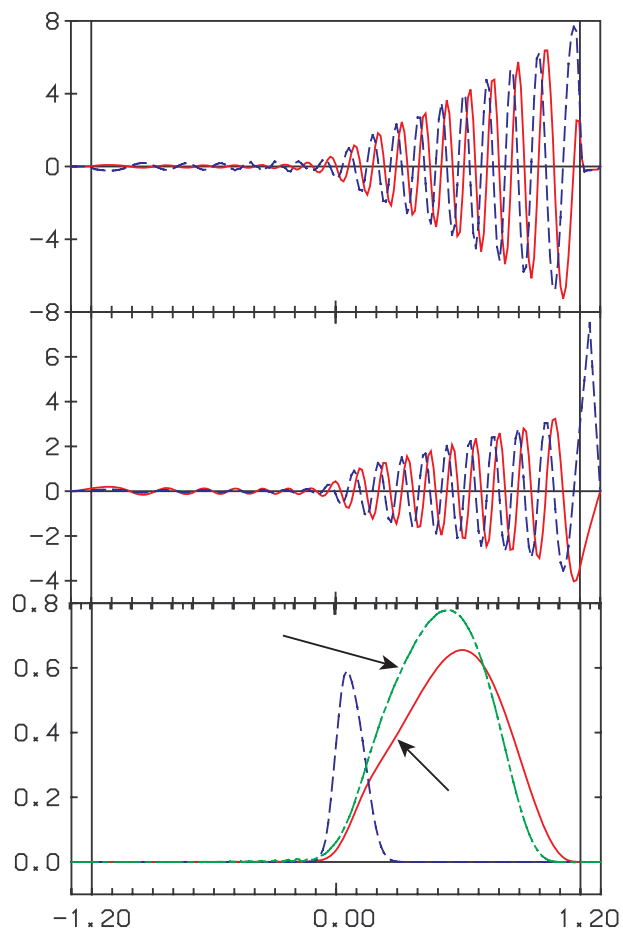
One-Dimensional Analysis (3)

ICRF minoring heating with α -particles ($n_D : n_{He} = 0.96 : 0.02$)

Differential form



Integral form



$$R_0 = 3.0\text{m}$$

$$a = 1.2\text{m}$$

$$B_0 = 3\text{T}$$

$$T_{e0} = 10\text{keV}$$

$$T_{D0} = 10\text{keV}$$

$$T_{\alpha 0} = 3.5\text{MeV}$$

$$n_{s0} = 10^{20}\text{m}^{-3}$$

$$\omega/2\pi = 45\text{MHz}$$

Absorption by α may be overestimated by differential approach.

2-D Formulation

- **Coordinates**

- **Magnetic coordinate system:** (ψ, χ, ζ)
- **Local Cartesian coordinate system:** (s, p, h)
- **Fourier expansion:** poloidal and toroidal mode numbers, m, n

- **Perturbed current**

$$\mathbf{J}(\mathbf{r}, t) = -\frac{q}{m} \int d\mathbf{v} q\mathbf{v} \int_{-\infty}^{\infty} dt' [\mathbf{E}(\mathbf{r}', t') + \mathbf{v}' \times \mathbf{B}(\mathbf{r}', t')] \cdot \frac{\partial f_0(\mathbf{v}')}{\partial \mathbf{v}'}$$

- **The time evolution of χ and ζ due to gyro-motion**

$$\begin{cases} \chi(t - \tau) = \chi(t) + \frac{\partial \chi}{\partial s} \frac{v_{\perp}}{\omega_c} \{\cos(\omega_c \tau + \theta_0) - \cos \theta_0\} + \frac{\partial \chi}{\partial p} \frac{v_{\perp}}{\omega_c} \{\sin(\omega_c \tau + \theta_0) - \sin \theta_0\} - \frac{\partial \chi}{\partial h} v_{\parallel} \tau \\ \zeta(t - \tau) = \zeta(t) + \frac{\partial \zeta}{\partial s} \frac{v_{\perp}}{\omega_c} \{\cos(\omega_c \tau + \theta_0) - \cos \theta_0\} + \frac{\partial \zeta}{\partial p} \frac{v_{\perp}}{\omega_c} \{\sin(\omega_c \tau + \theta_0) - \sin \theta_0\} - \frac{\partial \zeta}{\partial h} v_{\parallel} \tau \end{cases}$$

Variable Transformations

- **Transformation of Integral Variables**

- Transformation from the velocity space variables $(v_{\perp}, \theta_0)$ to the particle position s' and the guiding center position s_0 .

- Jacobian: $J = \frac{\partial(v_{\perp}, \theta_0)}{\partial(s', s_0)} = -\frac{\omega_c^2}{v_{\perp} \sin \omega_c \tau}$.

- Express $v_{\perp}$ and θ_0 by s' and s_0 using $\tau = t - t'$

$$v_{\perp}^2 = \left(\frac{s + s'}{2} - s_0 \right)^2 \frac{\omega_c^2}{\cos^2 \frac{1}{2} \omega_c \tau} + \left(\frac{s - s'}{2} \right)^2 \frac{\omega_c^2}{\sin^2 \frac{1}{2} \omega_c \tau} \equiv V_0^2$$

$$v_{\perp} \sin \theta_0 = \frac{\omega_c}{v_{\perp}} \frac{s - s'}{2} \frac{1}{\tan \frac{1}{2} \omega_c \tau} - \frac{\omega_c}{v_{\perp}} \left(\frac{s + s'}{2} - s_0 \right) \tan \frac{1}{2} \omega_c \tau \equiv V_1$$

$$v_{\perp} \sin(\omega_c \tau + \theta_0) = \frac{\omega_c}{v_{\perp}} \frac{s - s'}{2} \frac{1}{\tan \frac{1}{2} \omega_c \tau} + \frac{\omega_c}{v_{\perp}} \left(\frac{s + s'}{2} - s_0 \right) \tan \frac{1}{2} \omega_c \tau \equiv V_2$$

Integration over τ and $v_{\parallel}$

- **Maxwell distribution**

- Anisotropic Maxwell distribution with $T_{\perp}$ and $T_{\parallel}$:

$$f_0(s_0, \mathbf{v}) = n_0 \left(\frac{m}{2\pi T_{\perp}} \right)^{3/2} \left(\frac{T_{\perp}}{T_{\parallel}} \right)^{1/2} \exp \left[-\frac{v_{\perp}^2}{2v_{T_{\perp}}^2} - \frac{v_{\parallel}^2}{2v_{T_{\parallel}}^2} \right]$$

- **Integration over τ**

- Integral in time calculated by the Fourier series expansion with cyclotron period, $2\pi/\omega_c$

- **Integration over $v_{\parallel}$**

- Interaction between wave and particles along the magnetic field lines described by the plasma dispersion function.

Final Form of Induced Current

- Induced current:

$$\vec{\mu}^{-1} \cdot \begin{pmatrix} J_1^{mn}(\psi) \\ J_2^{mn}(\psi) \\ J_3^{mn}(\psi) \end{pmatrix} = \int du' \int du_0 \vec{\sigma}(u, u', u_0) \cdot \begin{pmatrix} E_1^{m'n}(\psi) \\ E_2^{m'n}(\psi) \\ E_3^{m'n}(\psi) \end{pmatrix}$$

- Electrical conductivity:

$$\vec{\sigma}(u, u', u_0) = -i \left(\frac{1}{2\pi} \right)^{\frac{7}{2}} n_0 \frac{q^2}{m} \sum_{m'n'} \sum_l \int_0^{2\pi} d\chi \int_0^{2\pi} d\zeta \exp i \{ (m' - m)\chi + (n' - n)\zeta \} \vec{H}(u, u', \chi)$$

- Matrix coefficients:

$$H_{1i} = (Q_3 \mu_{1i}^{-1} - u' Q_1 \mu_{2i}^{-1}) \frac{\sqrt{\pi}}{k_{\parallel} v_{T_{\parallel}}} Z(\eta_l) + \left[-\frac{Q_1 v_{T_{\perp}}}{v_{T_{\parallel}}^2} \mu_{3i}^{-1} + \left(1 - \frac{v_{T_{\perp}}^2}{v_{T_{\parallel}}^2} \right) \{ Q_3 \kappa_{2i} + Q_1 u' \kappa_{1i} \} \right] \sqrt{\frac{\pi}{2}} \frac{1}{k_{\parallel}} Z'(\eta_l)$$

$$H_{2i} = (-Q_2 u \mu_{1i}^{-1} + Q_0 u u' \mu_{2i}^{-1}) \frac{\sqrt{\pi}}{k_{\parallel} v_{T_{\parallel}}} Z(\eta_l) + \left[\frac{Q_0 u v_{T_{\perp}}}{v_{T_{\parallel}}^2} \mu_{3i}^{-1} - \left(1 - \frac{v_{T_{\perp}}^2}{v_{T_{\parallel}}^2} \right) u \{ Q_2 \kappa_{2i} + Q_0 u' \kappa_{1i} \} \right] \sqrt{\frac{\pi}{2}} \frac{1}{k_{\parallel}} Z'(\eta_l)$$

$$H_{3i} = \left(-\frac{Q_2}{v_{T_{\perp}}} \mu_{1i}^{-1} + \frac{Q_0 u'}{v_{T_{\perp}}} \mu_{2i}^{-1} \right) \sqrt{\frac{\pi}{2}} \frac{1}{k_{\parallel}} Z'(\eta_l) + \left[-\frac{Q_0}{v_{T_{\parallel}}} \mu_{3i}^{-1} + \frac{v_{T_{\parallel}}}{v_{T_{\perp}}} \left(1 - \frac{v_{T_{\perp}}^2}{v_{T_{\parallel}}^2} \right) \{ Q_2 \kappa_{2i} + Q_0 u' \kappa_{1i} \} \right] \frac{\sqrt{\pi}}{k_{\parallel}} \eta_l Z'(\eta_l)$$

Kernel Functions

- Kernel functions**

$$Q \begin{Bmatrix} 0 \\ 1 \\ 2 \\ 3 \end{Bmatrix} (u, u', \chi_0, l) = \int_0^{2\pi} d\lambda \frac{1}{|\sin \lambda|} \begin{Bmatrix} 1 \\ V_1 \\ V_2 \\ V_1 V_2 \end{Bmatrix} \times \exp i \left[\frac{k_{\perp} v_{T\perp}}{\omega_c} \{ (V_2 - V_1) \cos \alpha - (u - u') \sin \alpha \} + l\lambda - \frac{V_0^2}{2} \right]$$

$$V_0^2 = \left(\frac{u + u'}{2} \right)^2 \frac{1}{\cos^2 \frac{1}{2}\lambda} + \left(\frac{u - u'}{2} \right)^2 \frac{1}{\sin^2 \frac{1}{2}\lambda}$$

$$V_1 = \frac{u - u'}{2} \frac{1}{\tan \frac{1}{2}\lambda} - \frac{u + u'}{2} \tan \frac{1}{2}\lambda$$

$$V_2 = \frac{u - u'}{2} \frac{1}{\tan \frac{1}{2}\lambda} + \frac{u + u'}{2} \tan \frac{1}{2}\lambda$$

$$\overleftrightarrow{h} = \frac{1}{J\omega} \begin{pmatrix} 0 & -n & m' \\ n & 0 & i\frac{\partial}{\partial\psi} \\ -m' & -i\frac{\partial}{\partial\psi} & 0 \end{pmatrix}$$

$$u \equiv \frac{s - s_0}{v_{T\perp}} \omega_c$$

$$u' \equiv \frac{s' - s_0}{v_{T\perp}} \omega_c$$

where $\overleftrightarrow{\kappa} = \overleftrightarrow{\mu}^{-1} \cdot \overleftrightarrow{g} \cdot \overleftrightarrow{h}$, $\overleftrightarrow{\mu}$ is the transformation matrix for $(s, p, h) \rightarrow (\psi, \chi, \zeta)$, and $\overleftrightarrow{g}$ is the metric tensor.

Consistent Formulation of Integral Full Wave Analysis

- **Analysis of wave propagation**

- **Dielectric tensor:**

$$\nabla \times \nabla \times \mathbf{E}(\mathbf{r}) - \frac{\omega^2}{c^2} \int d\mathbf{r}_0 \int d\mathbf{r}' \frac{\mathbf{p}'}{m\gamma} \frac{\partial f_0(\mathbf{p}', \mathbf{r}_0)}{\partial \mathbf{p}'} \cdot \mathbf{K}_1(\mathbf{r}, \mathbf{r}', \mathbf{r}_0) \cdot \mathbf{E}(\mathbf{r}') = i \omega \mu_0 \mathbf{j}_{\text{ext}}$$

where $\mathbf{r}_0$ is the gyrocenter position.

- **Analysis of modification of momentum distribution function**

- **Quasi-linear operator**

$$\frac{\partial f_0}{\partial t} + \left(\frac{\partial f_0}{\partial \mathbf{p}} \right)_{\mathbf{E}} + \frac{\partial}{\partial \mathbf{p}} \int d\mathbf{r} \int d\mathbf{r}' \mathbf{E}(\mathbf{r}) \mathbf{E}(\mathbf{r}') \cdot \mathbf{K}_2(\mathbf{r}, \mathbf{r}', \mathbf{r}_0) \cdot \frac{\partial f_0(\mathbf{p}', \mathbf{r}_0, t)}{\partial \mathbf{p}'} = \left(\frac{\partial f_0}{\partial \mathbf{p}} \right)_{\text{col}}$$

- The kernels $\mathbf{K}_1$ and $\mathbf{K}_2$ are closely related and localized in the region $|\mathbf{r} - \mathbf{r}_0| \lesssim \rho$ and $|\mathbf{r}' - \mathbf{r}_0| \lesssim \rho$.

Summary

- **Toward an integrated full wave analysis in various range of frequencies, the integrated code, TASK, has been extended.**
- **Self-consistent analysis including modification of $f(p)$**
 - Full wave analysis with arbitrary velocity distribution was completed. Fokker-Planck analysis uses wave fields calculated by the full wave module. Preliminary result of self-consistent analysis was shown.
- **Full wave analysis of EC wave propagation in a small-size ST**
 - Tunneling through the cutoff layer and absorption on the upper hybrid layer were described.
- **2D full wave analysis including the FLR effects:**
 - 1D analysis elucidated the importance of the FLR effects. Formulation was extended to a 2D configuration. Implementation is under way.

Request for presentation

- **Please sign up you name and affiliation:**
(mail address from the List of Participants)

Future Plan of TASK Code

	Present Status	In 2 years	In 5 years
Equilibrium	Fixed/Free Boundary	Equilibrium Evolution	Start Up Analysis
Core Transport	1D Diffusive TR 1D Dynamic TR	Kinetic TR	2D Fluid TR
SOL Transport		2D Fluid TR	Plasma-Wall Interaction
Neutral Transport	1D Diffusive TR	Orbit Following	
Energetic Ions	Kinetic Evolution	Orbit Following	
Wave Beam	Ray/Beam Tracing	Beam Propagation	
Full Wave	Kinetic ϵ	Gyro Integral ϵ	Orbit Integral ϵ
Stabilities	Sawtooth Osc. ELM Model	Tearing Mode Resistive Wall Mode	Systematic Stability Analysis
Turbulent Transport	CDBM Model	Linear GK + ZF	Nonlinear ZK + ZF
		Diagnostic Module	
		Control Module	

Future Plan of Integrated Full Wave Analysis

- **DP**: dielectric tensor
 - **2D integral operator for Maxwellian**: under way
 - **2D integral operator for arbitrary $f(v)$** : planned
 - **Gyrokinetic arbitrary $f(v)$** : planned
- **WM**: full wave analysis
 - **Update to FEM version**: under way
 - **Waveguide excitation**: under way
- **FP**: Fokker-Planck analysis
 - **Integral quasi-linear operator**: formulation
 - **Radial diffusion**: Re-installation