

# ITER 運転シナリオのモデリング

福山 淳

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# 「定常運転」グループにおける ITER 運転シナリオ検討

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- **ITPA 「定常運転」グループ**

- 元「高エネルギー粒子・加熱・電流駆動」グループ
- 加熱・電流駆動による定常運転の維持
- 加熱・電流駆動装置の仕様策定に運転シナリオ検討が必要

- **ITPA 「閉じ込めデータベースとモデリング」グループ**

- ITER 物理 R&D 時代に輸送コードのベンチマークテスト  
→ **ITER Physics Basis**
- IAEA 2004 の際に統合モデリング会合
- 2006 春から統合モデリングコードの議論

# 經緯

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- **2005/05 (Como):**
  - **Joint activity to be agreed**
  - **ITER hybrid scenario, ITER steady-state scenario**
  - **Optimise scenarios based on their modelling**
  - **More Heating/CD (NBI, ECRH, ICRH) or install LHCD**
- **2005/11 (San Diego):**
  - **Modelling of ITER advanced scenarios**
  - **TSC, CRONOS, ONETWO, TASK**
  - **Standard set of initial conditions**
  - **Compare results from different codes**

# ITER Simulations

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- **Using the CDBM and CDBM05 models**
  - Both models could reproduce  $T_{e,i}$  profiles for L- and H-mode shots reasonably.
  - The prediction of high performance plasmas is anticipated with the CDBM05 model rather than the CDBM model.
- **Using simple heating and current drive models**
  - Power deposition profile is assumed.
  - Approximate analytic formula is assumed as a current drive efficiency.
- **Searching parameters predicting ITER operation scenarios**
  - Strong self-regulation of the plasma and nonlinearity of the transport model make it more difficult to predict the confinement performance.
- **In this simulation**
  - Density profiles are fixed as H-mode like profiles.
  - **TASK/TR is coupled with the 2-D equilibrium code, TASK/EQ.**
  - It solves the time evolution of the thermal transport and the magnetic diffusion.
  - Radiation losses caused by carbon and bremsstrahlung are taken into account ( $Z_{\text{eff}} \approx 1.5$ ).

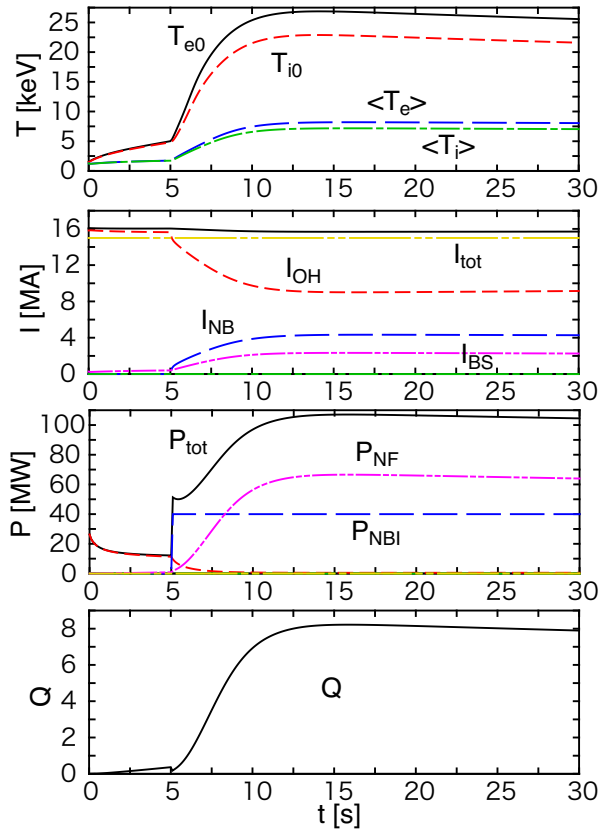
# High $Q$ Operational Scenario

- Large plasma current:  $I_p = 15$  MA, On-axis heating:  $P_{NB} = 40$  MW
- Positive shear profile, Relatively large  $f_{OH}$

CDBM

$$\beta_N = 1.49$$

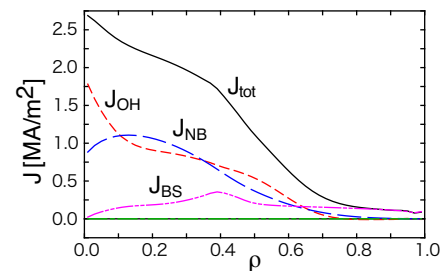
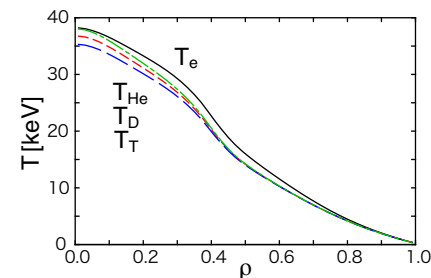
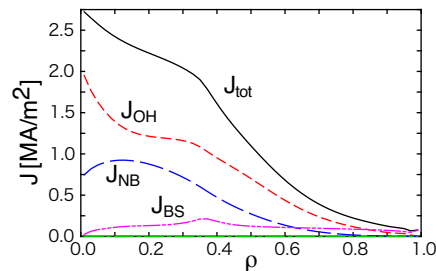
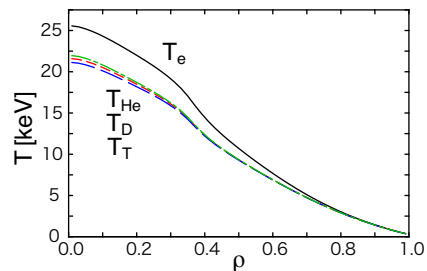
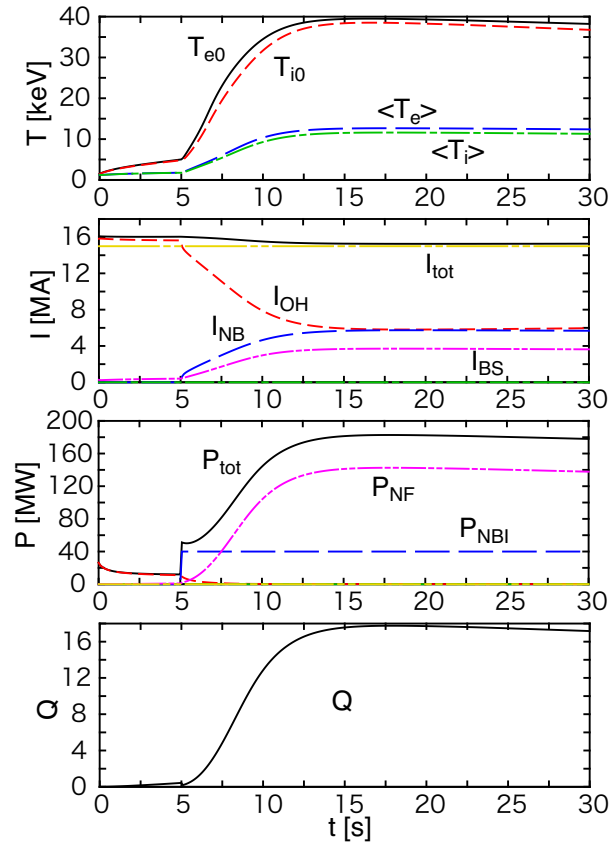
$$\tau_E = 3.0 \text{ s}$$



CDBM05

$$\beta_N = 2.63$$

$$\tau_E = 3.1 \text{ s}$$



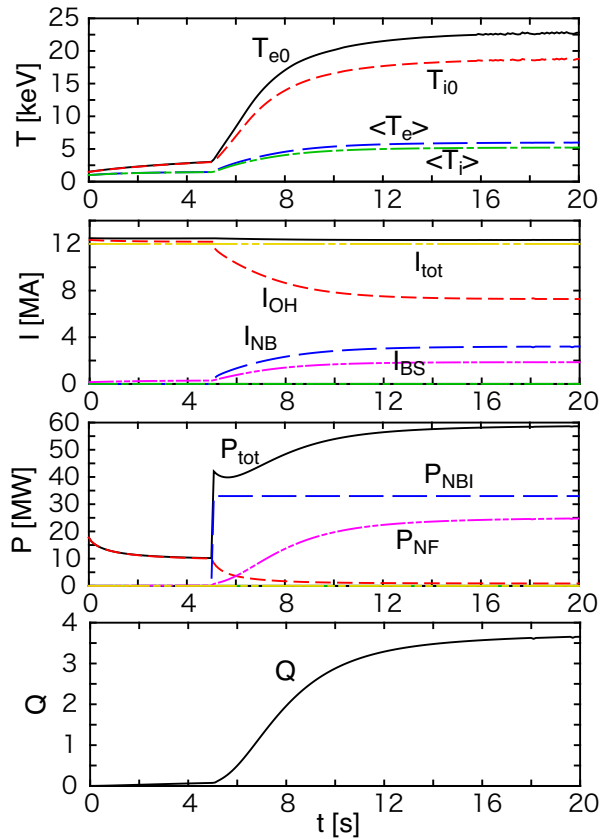
# Hybrid Operational Scenario

- Moderate plasma current:  $I_p = 12$  MA, On-axis heating:  $P_{NB} = 33$  MW
- Flat  $q$  profile with small ITB inside  $\rho = 0.4$

**CDBM**

$$\beta_N = 1.17$$

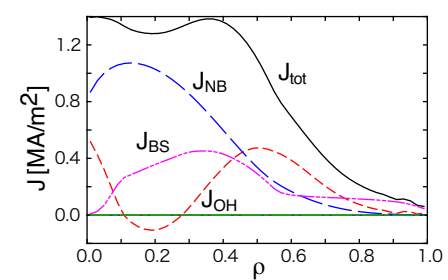
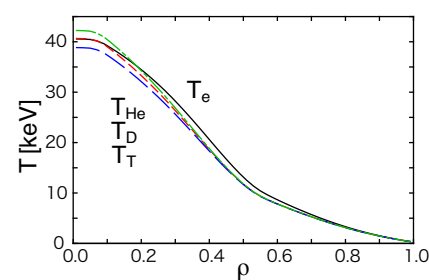
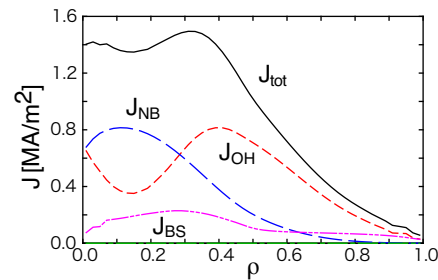
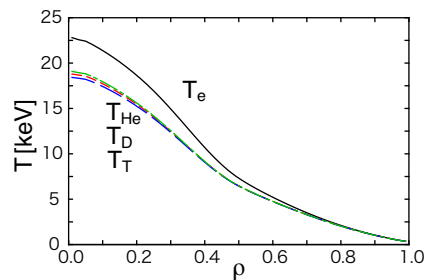
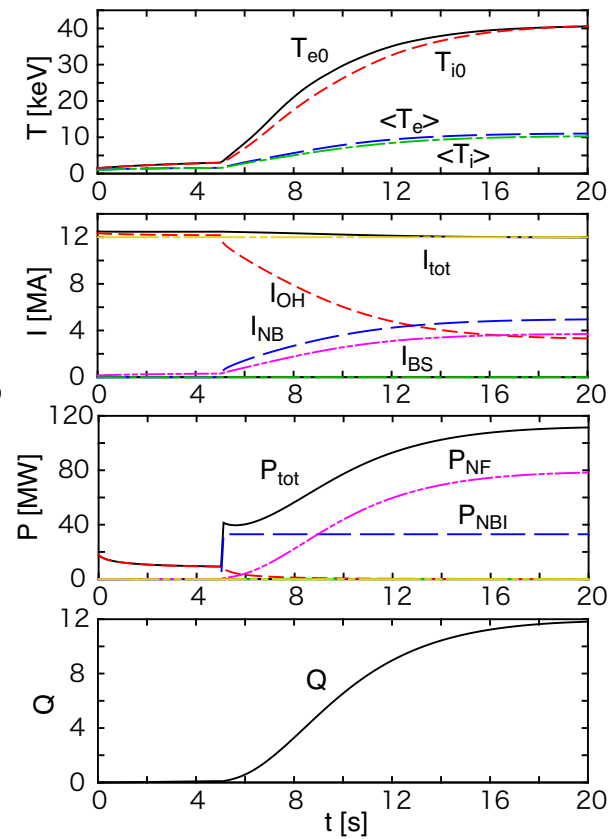
$$\tau_E = 3.1 \text{ s}$$



**CDBM05**

$$\beta_N = 2.58$$

$$\tau_E = 3.6 \text{ s}$$



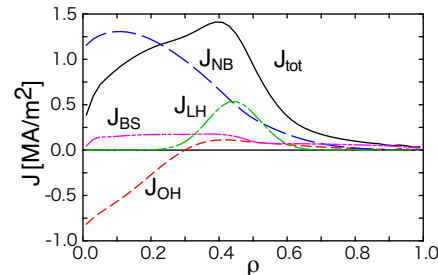
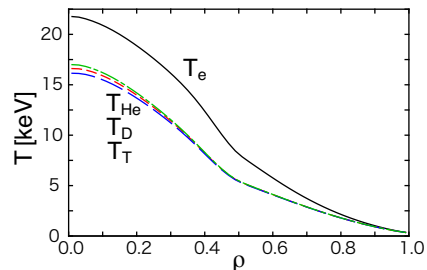
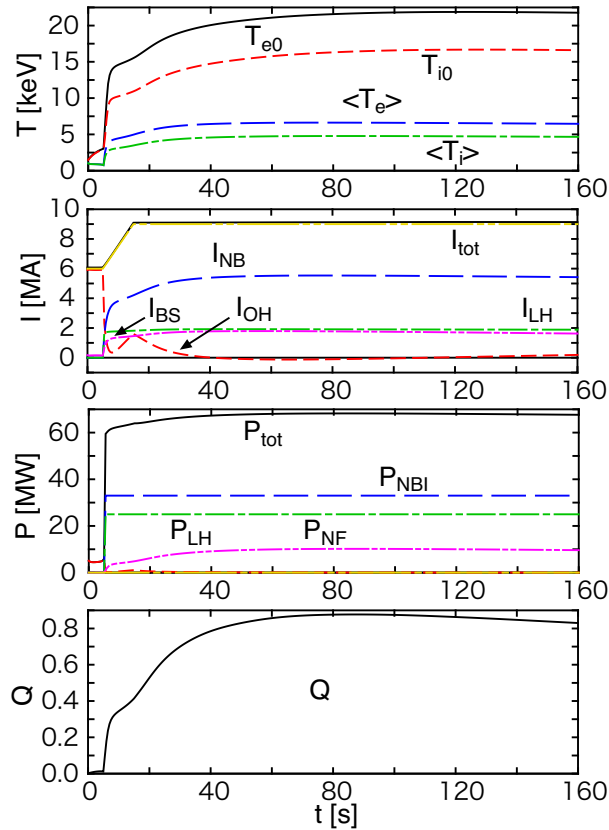
# Quasi-Steady State Operational Scenario

- $I_p = 6 \rightarrow 9$  MA for 10 s, Negative shear profile,  $I_{OH} \sim 0$

CDBM

$$\beta_N = 1.2$$

$$\tau_E = 3.0 \text{ s}$$



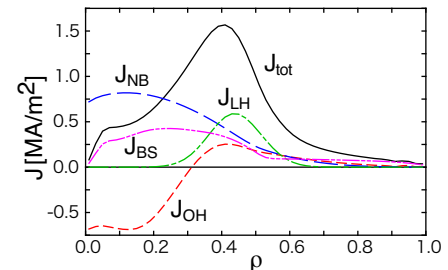
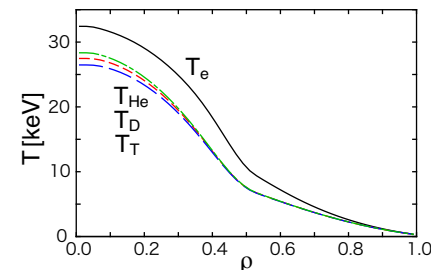
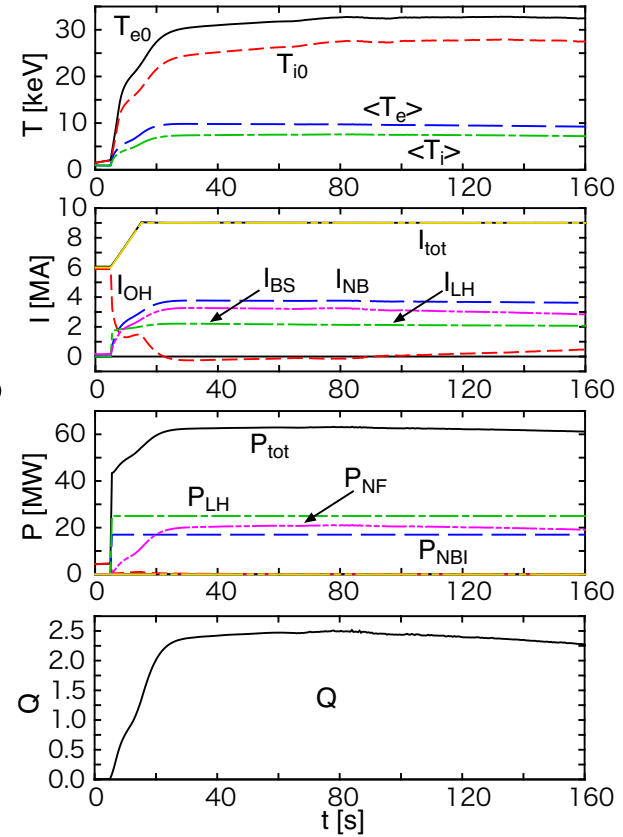
$$P_{NB} = 35 \text{ MW}$$

$$P_{LH} = 30 \text{ MW}$$

CDBM05

$$\beta_N = 1.55$$

$$\tau_E = 3.2 \text{ s}$$

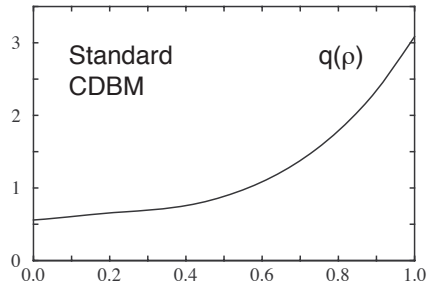


$$P_{NB} = 17 \text{ MW}$$

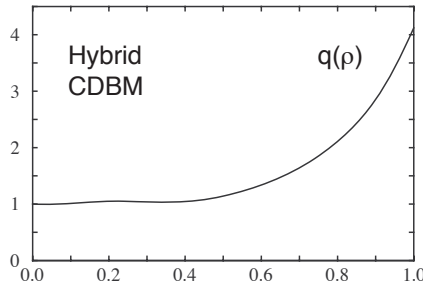
$$P_{LH} = 25 \text{ MW}$$

# $q$ Profiles of Previous Shots

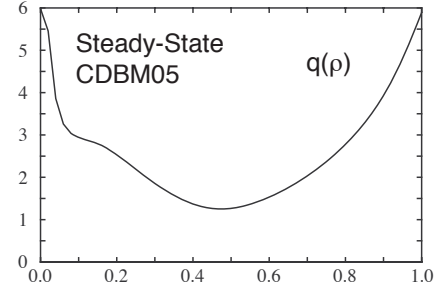
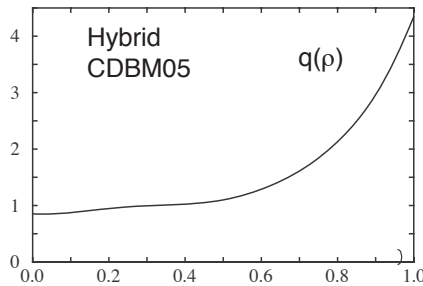
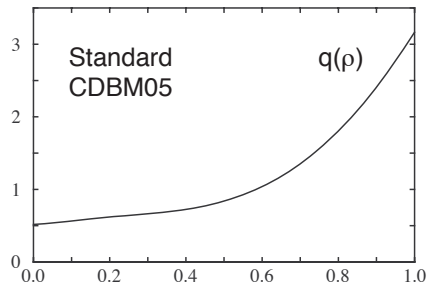
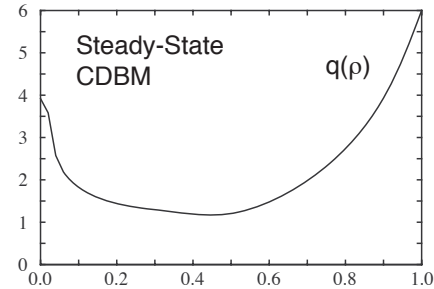
## Standard



## Hybrid



## Steady State



- Control of current profile in the hybrid operation requires more improvement to keep  $q(0) > 1$ .
- Performance of the quasi steady-state operation will be improved if the H-mode plasma edge (edge transport barrier) are included. .



# ITPA-SSO: 2006/04 (Naka)

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- **ITER simulation results**
  - TSC (Kessel)
  - ONETWO (Murakami)
  - CRONOS (Giruzzi)
  - TOPICS (Hayashi)
  - TASK (Fukuyama)
- **Simulation guideline**
  - Hybrid scenario
  - Steady-state scenario

# “Guideline” SS Scenario Parameters

April 13 2006

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Plasma in flattop phase (as stationary as possible)

$$I_p = 9 \text{ MA}$$

$$B_T = 5.3 \text{ T}$$

$$\tau_P^*/\tau_E = 5.0$$

$$f_D/(f_D+f_T) = 0.5$$

$$f_{Be} = 2\%$$

$$f_{Ar} = 0.12\%$$

$$P_{NBI} = 33 \text{ MW (1 MeV, off-axis)}$$

$$P_{ICRF} = 20 \text{ MW (40 MHz, FWCD phasing)}$$

$$P_{EC} = 20 \text{ MW (170 GHz, midplane, } \theta_{tor} = ??)$$

$R_b, Z_b$  for fixed boundary  
(also PF coil currents,  $li$ ,  $\beta_p$  for free-boundary)

$$\rho_{ped}^{\text{density}} = 0.8$$

$$\rho_{ped}^{\text{temperature}} = 0.88$$

$$n_{ped} = n(\rho = 0.90) = n(0)$$

$$T_{ped} = 10.0 \text{ keV}$$

$$n(0) = 0.85 \times 10^{20} / \text{m}^3$$

$$n(\rho = 0.0 - 0.8) = n(0)$$

Linear drop from  $\rho = 0.8 - 1.0$

$$n(\rho = 1.0) = 1.0 \times 10^{20} / \text{m}^3$$

$$T(\rho = 1.0) = 200 \text{ eV}$$

$n_z(\rho)/n_z(0)$  same as electrons

$T_e(\rho)$  and  $T_i(\rho)$  profiles from GLF23

$T_z(\rho)$  same as fuel ions

# “Guideline” Hybrid Scenario Parameters

April 13, 2006

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Plasma in flattop phase (as stationary as possible)

$$I_p = 12 \text{ MA}$$

$$B_T = 5.3 \text{ T}$$

$$\tau_P^*/\tau_E = 5.0$$

$$f_D/(f_D+f_T) = 0.5$$

$$f_{Be} = 2\%$$

$$f_{Ar} = 0.12\%$$

$$P_{NBI} = 33 \text{ MW (1 MeV, off-axis)}$$

$$P_{ICRF} = 10 \text{ MW (53 MHz, heating only)}$$

$$P_{EC} = 20 \text{ MW (170 GHz, midplane launch, } \theta_{tor} = ??)$$

$R_b, Z_b$  for fixed boundary  
(also PF coil currents,  $li$ ,  $\beta_p$  for free-boundary)

$$\rho_{ped} = 0.925$$

$$n_{ped} = n(\rho = 0.925) = n(0)$$

$$T_{ped} = 7.0 \text{ keV}$$

$$n(0) = 0.95 \times 10^{20} / \text{m}^3$$

$$n(\rho = 0.0 - 0.925) = n(0)$$

Linear drop from  $\rho = 0.925 - 1.0$

$$n(\rho = 1.0) = 0.35 \times n(0)$$

$$T(\rho = 1.0) = 200 \text{ eV}$$

$$n_z(\rho)/n_z(0) \text{ same as electrons}$$

$T_e(\rho)$  and  $T_i(\rho)$  profiles from GLF23

$T_z(\rho)$  same as fuel ions

# ITPA-SSO: 2006/10 (Chengdu)

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- **IAEA Fusion Energy conference**
  - **Simulation of the Hybrid and Steady State Advanced Operating Modes in ITER**
    - **C. E. Kessel et al. (ITPA-SSO TG)**
    - **Benchmark test:**
    - **CRONOS, ONETWO, TSC/TRANSP, TOPICS, and ASTRA**
- **ITPA SSO TG**
  - **Modelling of ITER advanced scenarios**
    - **TSC/TRANSP (C. Kessel)**
    - **CRONOS (G. Giruzzi)**
  - **Actuator benchmark test**
    - **ECCD, LHCD, ICRH, NBI**

# ITER Hybrid Benchmark Simulations

*(more work is needed to strictly enforce these prescriptions for the simulations)*

**Plasma in flattop phase (as stationary as possible)**

**$I_p = 12$  MA**

**$B_T = 5.3$  T**

**$t_p^*/t_E = 5.0$**

**$f_D/(f_D+f_T) = 0.5$**

**$f_{Be} = 2\%$**

**$f_{Ar} = 0.12\%$**

**$P_{NBI} = 33$  MW (1 MeV, off-axis,  $Z_{NBcenter} = -0.42$  m @  $R = 5.3$  m)**

**$P_{ICRF} = 20$  MW (53 MHz, heating only, 2T)**

**$P_{EC} = 20$  MW (170 GHz, midplane launch,  $\alpha_{1,2,3} = 0^\circ$ ,  $\beta_{1,2,3} = 30^\circ$ ,  $P_{1,2,3} = 6.67$  MW)**

**$R_b, Z_b$  for fixed boundary (also PF coil currents,  $I_i$ ,  $\beta_p$  for free-boundary)**

**$\rho_{ped} = 0.925$**

**$n_{ped} = n(\rho = 0.925) = n(0)$**

**$T_{ped} = 5.0$  keV**

**$n(0) = 0.85 \times 10^{20}$  /m<sup>3</sup>**

**$n(\rho = 0.0 - 0.925) = n(0)$**

**Linear drop from  $\rho = 0.925 - 1.0$**

**$n(\rho = 1.0) = 0.35 \times n(0)$**

**$T(\rho = 1.0) = 200$  eV**

**$n_z(\rho)/n_z(0)$  same as electrons**

**$Te(\rho)$  and  $Ti(\rho)$  profiles from GLF23**

**$T_z(r)$  same as fuel ions**

**Hybrid #1) NB + IC**

**Hybrid #2) NB + IC + EC**

# ITER Hybrid NB + IC

	li(1)	q(0)	$W_{th}$ (MJ)	$\beta_N$	$H_{98}^*$	Te(0) (keV)	Ti(0) (keV)	$Z_{eff}$	$I_{BS}$ (MA)	$I_{NB}$ (MA)	$P_\alpha$ (MW) Q
<b>ONETWO</b>	0.72*	0.58	295	2.10	1.10	27.2	33.4	1.70	3.87	2.07	69 6.5
<b>TSC/ TRANSP</b>	1.05	0.44	340	2.18	1.41 1.18	33.8	33.8	1.71	3.39	1.42	80 7.5
<b>CRONOS</b>	0.70*	0.69	339	2.30	1.43	26.3	25.6	1.69	4.26	0.92	87.6 8.3
<b>TOPICS</b>	0.61*	0.99	359	2.24	1.05	30.4	31.6	1.70	3.93	2.62	82.2 7.8
<b>ASTRA</b>	0.77*	0.53	327	2.12	1.18	34.3	34.5	1.71	2.82	1.92	99.7 9.4

\*These are li(3)

\*Higher  $H_{98}$  values use  $P_{input}$  and lower values use  $(P_{input} - P_{rad})$

# Benchmark Test for ITER Hybrid Scenario

- **C.E. Kessel et al.: IAEA2006 IT/P1-7 (ITPA/SSO)**
- Codes: **CRONOS, ONETWO, TSC/TRANSP, TOPICS, ASTRA**

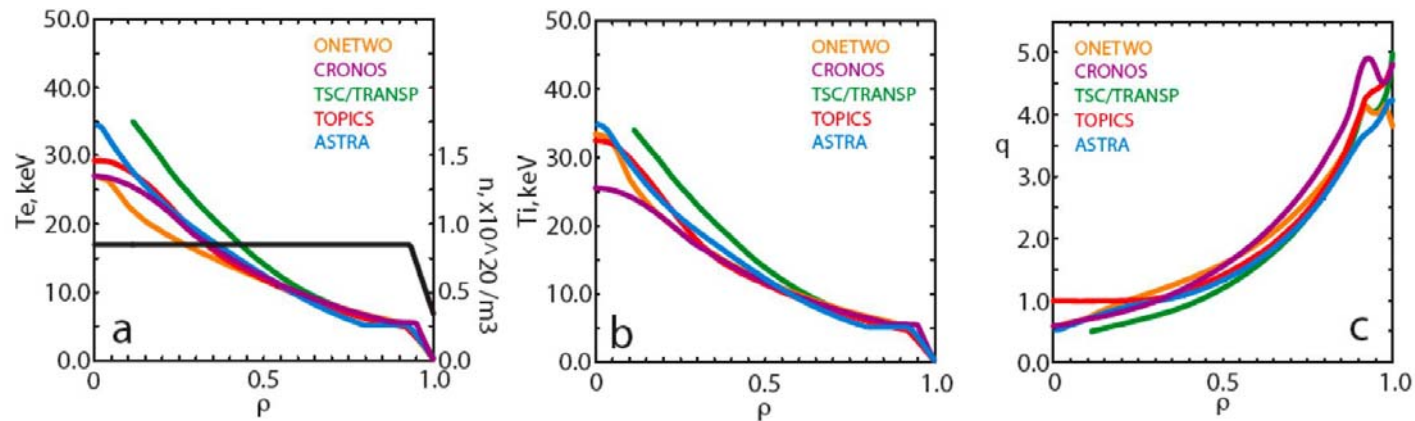


Figure 1. Electron temperature profiles and density profile (a), ion temperature profiles (b), safety factor profiles (c), for the NB+IC ITER Hybrid simulations.

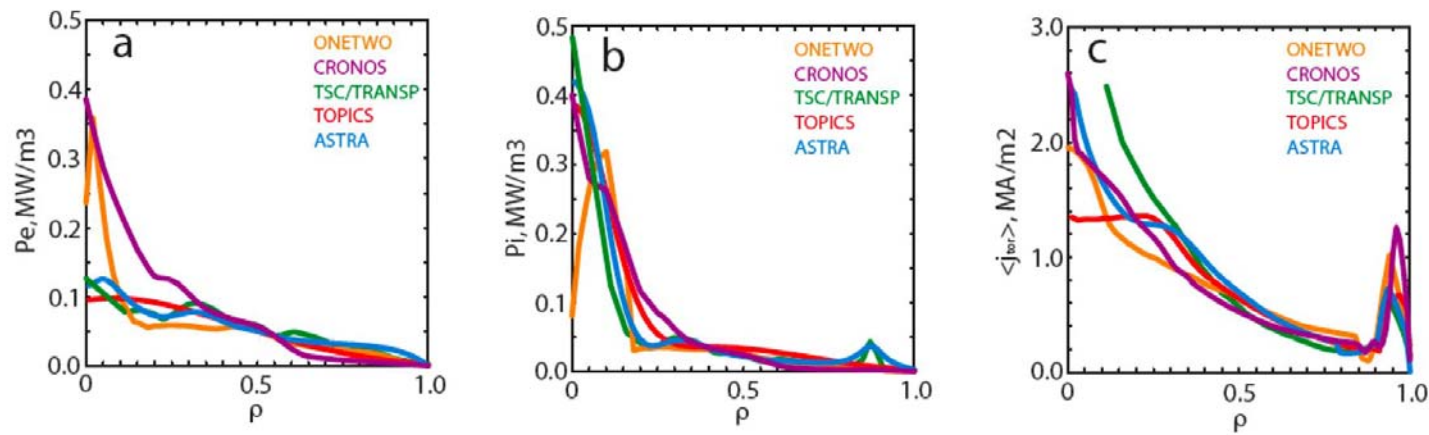


Figure 2. External power deposition profiles to electrons (a) and ions (b) and the toroidal current density (c) for the NB+IC ITER Hybrid simulations.

# Benchmark Test for ITER Steady-State Scenario

- Codes: **TOPICS, CRONOS, TSC/TRANSP**

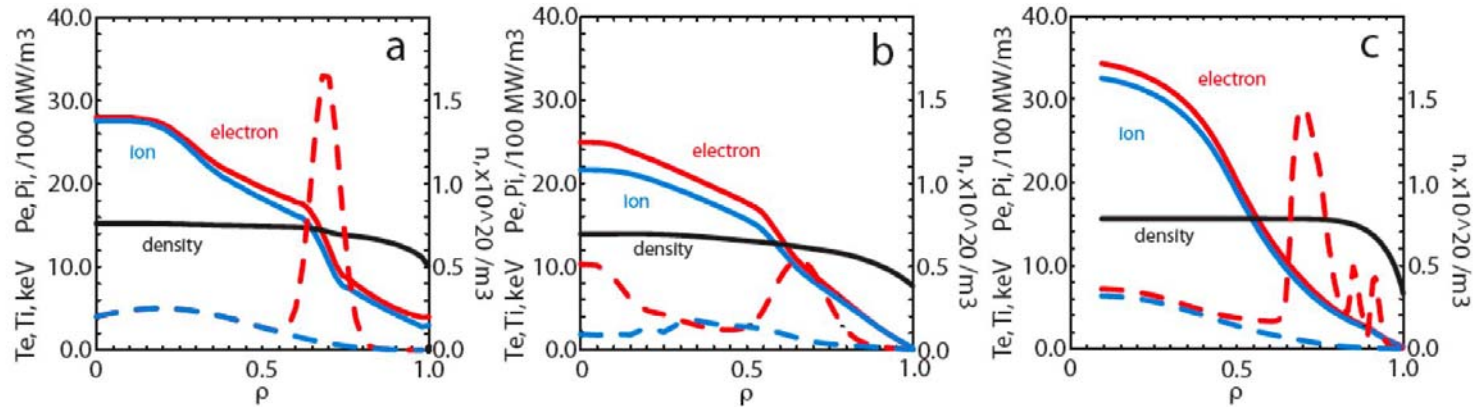


Figure 5. Electron and ion temperature, density, and external power deposition profiles for Steady State ITER simulations, (a) TOPICS (NB+EC), (b) CRONOS (NB+IC+LH), and (c) TSC/TRANSP (NB+IC+LH).

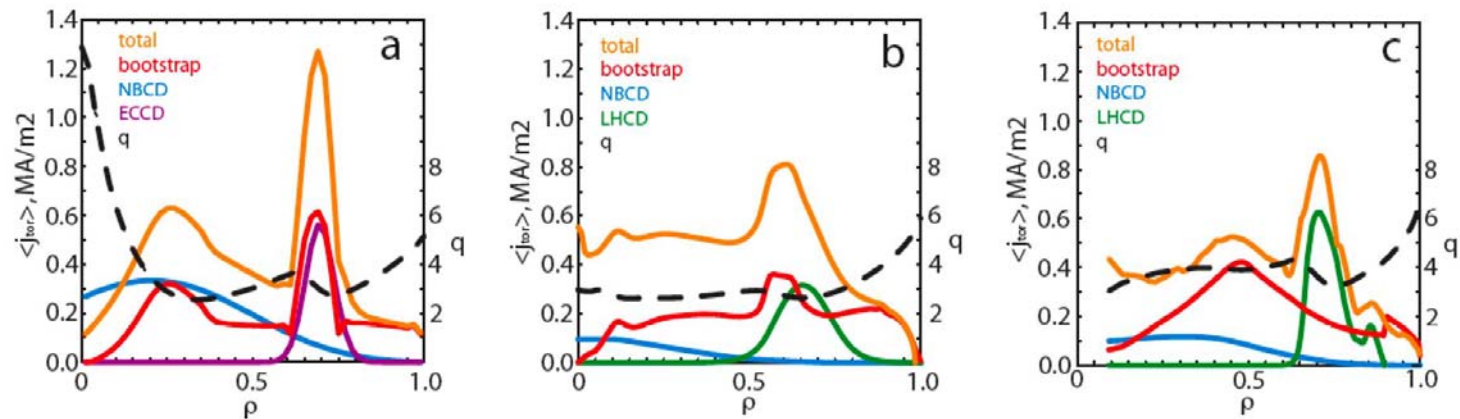


Figure 6. Safety factor and toroidal current density profiles and its contributions for Steady State ITER simulations, (a) TOPICS (NB+EC), (b) CRONOS (NB+IC+LH), and (c) TSC/TRANSP (NB+IC+LH).



# 今後の課題

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- **ITER 運転シナリオのモデリング**
  - **CDBM Modeling group** との連携
  - シミュレーション ガイドラインの再検討
  - 加熱機構モデリング
  - ベンチマークテストの意義
- **日本の貢献**
  - 運転シナリオモデリング： **TOPICS, TASK**
  - 加熱機構ベンチマークテスト： **ECCD, NNBI**
  - **SSO-TG** 会合に出席しつづけることが必要
- **次回：2007/05/9-11**